



Standard Test Method for Determination of Sulfur Compounds in Natural Gas and Gaseous Fuels by Gas Chromatography and Chemiluminescence¹

This standard is issued under the fixed designation D5504; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This test method is primarily for the determination of speciated volatile sulfur-containing compounds in high methane content gaseous fuels such as natural gas. It has been successfully applied to other types of gaseous samples including air, digester, landfill, and refinery fuel gas. The detection range for sulfur compounds, reported as picograms sulfur, is ten (10) to one million (1 000 000). This is equivalent to 0.01 to 1 000 mg/m³, based upon the analysis of a 1 cc sample.

1.2 The range of this test method may be extended to higher concentration by dilution or by selection of a smaller sample loop.

NOTE 1— Dilution will reduce method precision.

1.3 This test method does not purport to identify all sulfur species in a sample. Only compounds that are eluted through the selected column under the chromatographic conditions chosen are determined. The detector response to sulfur is equimolar for all sulfur compounds within the scope (1.1) of this test method. Thus, unidentified compounds are determined with equal precision to that of identified substances. Total sulfur content is determined from the total of individually quantified components.

1.4 The values stated in SI units are standard. The values stated in inch-pound units are for information only.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

¹ This test method is under the jurisdiction of ASTM Committee D03 on Gaseous Fuels and is the direct responsibility of Subcommittee D03.05 on Determination of Special Constituents of Gaseous Fuels.

Current edition approved June 15, 2008. Published July 2008. Originally approved in 1994. Last previous edition approved in 2006 as D5504 – 01(2006). DOI: 10.1520/D5504-08.

2. Referenced Documents

2.1 ASTM Standards:²

D1072 Test Method for Total Sulfur in Fuel Gases by Combustion and Barium Chloride Titration

D1945 Test Method for Analysis of Natural Gas by Gas Chromatography

D3609 Practice for Calibration Techniques Using Permeation Tubes

D4468 Test Method for Total Sulfur in Gaseous Fuels by Hydrogenolysis and Rateometric Colorimetry

E594 Practice for Testing Flame Ionization Detectors Used in Gas or Supercritical Fluid Chromatography

3. Summary of Test Method

3.1 The analysis of gaseous sulfur compounds is challenging due to the reactivity of these substances. They are difficult to sample and analyze. Ideally, analysis is performed on-site to eliminate sample deterioration as a factor in analysis. Sampling must be performed using non-reactive containers, such as Silcosteel³ lined vessels, Tedlar⁴ bags with polypropylene fittings or the equivalent. Tedlar⁴ bag samples require protection from light and heat. Laboratory equipment must be inert or passivated to ensure reliable results.

3.2 A one cc (mL) sample is injected into a gas chromatograph where it is eluted through a megabore, thick film, methyl silicone liquid phase, open tubular partitioning column or other suitable column, and separated into its individual constituents.

3.3 *Sulfur Chemiluminescence Detection*—As sulfur compounds elute from the gas chromatographic column, they are processed in a flame ionization detector (FID) or a heated combustion zone. The products are collected and transferred to a sulfur chemiluminescence detector (SCD). This technique provides a sensitive, selective, linear response to volatile sulfur

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Silcosteel is a trademark of Restek Corporation, 110 Benner Circle Bellefonte, PA, 16823.

⁴ Tedlar is a trademark of DuPont.

compounds and may be used while collecting hydrocarbon and fixed gas data from a FID.

3.3.1 *Detectors in Series with a SCD*—A SCD can frequently be used in series with other fixed gas and hydrocarbon detectors. However, regulatory bodies may question detector compatibility and require demonstration of equivalence between a SCD in a multi-detector system and a SCD operated using a FID or combustion zone. The user is referred to USEPA Method 301 for an example of a general equivalence procedure.

3.3.2 *Alternative Detectors*—This test method is written for the sulfur chemiluminescent detector but other sulfur specific detectors can be used provided they have sufficient sensitivity, respond to all eluted sulfur compounds, do not suffer from interferences and satisfy quality assurance criteria. Regulatory agencies may require demonstration of equivalency of alternative detection systems to the SCD.

4. Significance and Use

4.1 Many sources of natural and petroleum gases contain sulfur compounds that are odorous, corrosive, and poisonous to catalysts used in gaseous fuel processing.

4.2 Low ppm amounts of sulfur odorants are added to natural gas and LP gases for safety purposes. Some odorants are unstable and react to form compounds having lower odor thresholds. Quantitative analysis of these odorized gases ensures that odorant injection equipment is performing to specification.

4.3 Although not intended for application to gases other than natural gas and related fuels, this test method has been successfully applied to fuel type gases including refinery, landfill, cogeneration, and sewage digester gas. Refinery, landfill, sewage digester and other related fuel type gases inherently contain volatile sulfur compounds that are subject to federal, state, or local control. The methane fraction of these fuel type gases are occasionally sold to distributors of natural gas. For these reasons, both regulatory agencies and production and distribution facilities may require the accurate determination of sulfur to satisfy regulatory, production or distribution requirements. Fuel gases are also used in energy production or are converted to new products using catalysts that are poisoned by excessive sulfur in the feed gas. Industry frequently requires measurement of sulfur in these fuel type gases to protect their catalyst investments.

4.4 *Analytical Methods*—Gas chromatography (GC) is commonly used in the determination of fixed gas and organic composition of natural gas (Test Method [D1945](#)). Other standard ASTM methods for the analysis of sulfur in fuel gases include Test Methods [D1072](#) and [D4468](#) for total sulfur and Test Methods [D4010](#) and [D4884](#) for hydrogen sulfide.

5. Apparatus

5.1 *Chromatograph*—Any gas chromatograph of standard manufacture, with hardware necessary for interfacing to a chemiluminescence detector and containing all features necessary for the intended application(s) can be used. Chromatographic parameters must be capable of obtaining retention time repeatability of 0.05 min (3 s) throughout the scope of this analysis.

5.1.1 *Sample Inlet System*—A sample inlet system capable of operating continuously at the maximum column temperature is used. A split/splitless injection system capable of splitless operation and split control from 10:1 up to 50:1 may be used with capillary columns, or when interferants are encountered. An automated gas sampling valve is required for many applications. The inlet system must be conditioned or constructed of inert material and evaluated frequently for compatibility with trace quantities of reactive sulfur compounds.

5.1.2 *Carrier and Detector Gas Control*—Constant flow control of carrier and detector gases is critical for optimum and consistent analytical performance. Control is achieved by use of pressure regulators and fixed flow restrictors. The gas flow is measured by appropriate means and adjusted. Mass flow controllers, capable of maintaining gas flow constant to $\pm 1\%$ at the flow rates necessary for optimal instrument performance can be used.

5.1.3 *Detector*—Sulfur compounds are processed using a flame ionization detector (FID), a heated combustion zone or a similar device. The products are collected and delivered to a sulfur chemiluminescence detector (SCD).

5.1.3.1 *FID*—The detector must meet or exceed the specifications in Table 1 of Practice [E594](#) while operating within manufacturers specifications. The detector must be capable of operating at the maximum column temperature. The flow path from the injection system through the column to the FID must remain at or above the column temperature throughout the analysis. The FID must allow for the insertion of a SCD sampling probe into the flame without compromising the ability of the FID to detect hydrocarbons. Flow rates of air and hydrogen or, alternatively of oxygen and hydrogen, must be optimized to produce a hydrogen rich flame or combustion zone that is capable of combusting hydrocarbons. This is necessary to minimize matrix effects. When performing the simultaneous detection of hydrocarbons is necessary, a FID and heated combustion zone can be used in series. Zero air is necessary when performing the simultaneous determination of sulfur gases and hydrocarbons.

5.1.3.2 *SCD*—The sulfur chemiluminescence detector shall meet or exceed the following specifications: (1) greater than 10^5 linearity, (2) less than 5 pg S/s sensitivity, (3) greater than 10^6 selectivity for sulfur compounds over hydrocarbons, (4) no quenching of sulfur compound response, and (5) no interference from co-eluting compounds at the usual GC sampling volumes.

5.1.3.3 *Heated Combustion Zone*—Sulfur compounds eluting from the chromatographic column are processed in a heated hydrogen rich combustion zone or a flame ionization detector fitted to the end of the column. Products are transferred under reduced pressure to the reaction chamber of a chemiluminescence detector. An excess of ozone present in the chamber reacts with the sulfur combustion product(s) to liberate blue (480 nm) and ultraviolet light (260 nm).

5.1.3.4 *SCD operation* is based on the chemiluminescence (light emission) produced by the reaction of ozone with an unidentified sulfur species produced in a combustion zone, flame ionization detector or related device. The chemiluminescent sulfur species is the subject of on-going research. The

passing over the tubes. These calibration gases are used to calibrate the GC/SCD system.

6.1.1.1 *Permeation System Temperature Control*—Permeation devices are maintained at the calibration temperature within 0.1°C.

6.1.1.2 *Permeation System Flow Control*—The permeation flow system measures diluent gas flow over the permeation tubes within ±2 percent.

6.1.1.3 Permeation tubes are inspected and weighed to the nearest 0.01 mg on at least a monthly basis using a balance calibrated against NIST traceable “S” class weights or the equivalent. Analyte concentration is calculated by weight loss and dilution gas flow rate as per Practice D3609. These devices are discarded when the liquid contents are reduced to less than ten (10) percent of the initial volume or when the permeation surface is unusually discolored or otherwise compromised.

6.2 *Compressed Gas Standards*—Alternatively, blended gaseous sulfur standards in nitrogen, helium or methane base gas may be used. Care must be exercised in the use of compressed gas standards since they can introduce errors in measurement due to lack of uniformity in their manufacture or instability in their storage and use. The protocol for compressed gas standards contained in the appendix can be used to ensure uniformity in compressed gas standard manufacture and provide for traceability to a NIST or NMI reference material.

6.2.1 Compressed gas standard regulators must be appropriate for the delivery of sulfur gases and attached fittings must be passivated or inert to sulfur gases.

6.2.2 The following sulfur compounds are recommended for inclusion in a compressed gas standard.

- Hydrogen sulfide (H₂S)
- Carbonyl sulfide (COS)
- Methyl mercaptan (CH₃SH)

6.2.3 The following substances can also be included in a compressed gas standard.

- Ethyl mercaptan (CH₃CH₂SH)
- 1-propanethiol (CH₃CH₂CH₂SH)
- 2-propanethiol (CH₃CHSHCH₃)
- Dimethyl sulfide (CH₃SCH₃)

6.2.4 The following compounds are not recommended for inclusion in mixed component standards due to their potential for promoting degradation.

- Carbon disulfide (CS₂)
- Dimethyl disulfide (CH₃SSCH₃)
- Other disulfides

6.2.5 All multicomponent compressed gas standards must be re-certified as recommended by the manufacturer or as needed to insure accuracy.

6.2.6 For the analysis of complex samples, such as refinery fuel and related fuel type gases, the SCD system must demonstrate the capability of eluting common relatively high molecular weight volatile sulfur compounds including di-n-propyl sulfide (propyl sulfide). A retention time standard for demonstrating this capability can be prepared from the compound (ACS Grade) at approximately 160 ppmv concentration by addition of a 1 µL aliquot of the liquid to a 10 L Tedlar bag filled with UHP nitrogen or helium.

6.2.7 *Carrier Gas*—Helium or nitrogen of high purity. Use of molecular sieves or other suitable agents to remove water,

oxygen, and hydrocarbons is recommended. Gas pressure must be sufficient to ensure a constant carrier flow rate (see 5.1.2).

6.2.8 *Hydrogen*—High purity hydrogen is required as fuel for a flame ionization detector, a heated combustion zone or a similar device.

6.2.9 *Air*—High purity air is required as oxidant for a flame ionization detector, a heated combustion zone or a similar device.

6.2.10 *Oxygen*—High purity oxygen supply gas to the SCD ozone generator may be used for maximum detector sensitivity.

7. Equipment Preparation

7.1 *Chromatograph*—Place in service in accordance with the manufacturer’s instructions. Many operating conditions can be used to perform sulfur gas speciation and quantitation. Typical, minimal performance criteria for chromatographic conditions are:

7.1.1 The conditions must separate all volatile sulfur compounds required for calibration.

7.1.2 Chromatographic conditions must elute all sulfur species of interest.

7.1.3 The injection system must transfer without loss or absorption all sulfur compounds of interest to the GC column without reaction between sulfur species or excessive carryover between samples.

7.1.4 The operating conditions presented in Table 1 have been successfully used to fulfill the above criteria. Table 1 provides a listing of the retention times of selected sulfur compounds obtained using the parameters in Table 2. Figs. 2 and 3 illustrate typical analyses of a standard mixture and natural gas.

7.2 *SCD*—Place in service in accordance with the manufacturer’s instructions. FID, heated combustion zone, and mixed FID/heated combustion zone interface configurations can be successfully applied to the analysis of sulfur gases in gaseous samples. For each of these interface configurations, optimization of the oxidant/fuel ratio is critical for ensuring complete combustion of hydrocarbon components in a sample. A flame or combustion zone that is too hydrogen rich will result in incomplete combustion and will produce a methane peak before elution of H₂S (Fig. 4). Matrix interference is occasionally observed when changing sample size. Matrix interference is also indicated by recoveries less than 90 % or greater than 110 % for samples spiked with calibration gas or samples

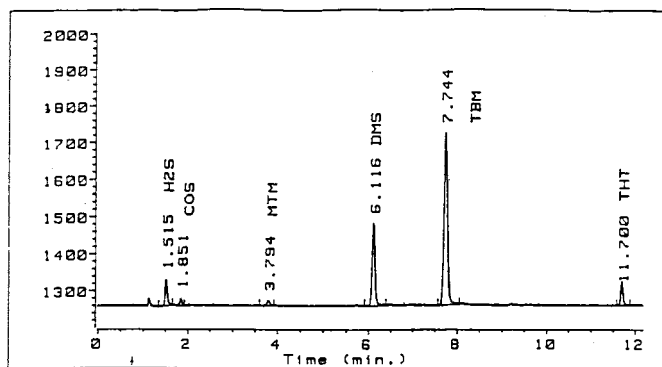


FIG. 2 Natural Gas Analysis-Sulfur Compounds

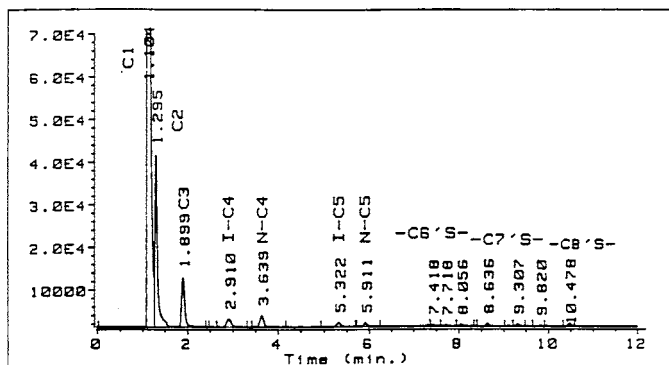


FIG. 3 Natural Gas Analysis-Hydrocarbon Compounds

diluted with air. When matrix interference is indicated, samples may be analyzed by dilution or application of other mitigation efforts provided a spiked sample performed using the mitigation procedure results in recoveries within 10 % of theoretical results. Operational features specific to the interface configuration employed are described in the following.

7.2.1 *FID Interface*—Placed into service as per the SCD manufacturers instructions. For this interface, probe placement is critical for optimal sensitivity and reproducibility. Response that remains the same or decreases with increasing sample size, indicates questionable interface efficiency (Figs. 5 and 6).

7.2.2 *Flameless Interface or Other Heated Combustion Zone*—Placed into service as per manufacturers instructions. The typical flameless/combustion zone interface contains ceramic tubes in its construction. The performance of these tubes is critical to performance of the SCD system. Compromised ceramic tubes are susceptible to matrix effects. Compromised tubes may allow for reproducible duplicate sample analysis but will fail QA procedures such as matrix dilution and spike analyses. Poorly functioning tubes can also result in severe instrument drift, loss of equimolar response and general response instability. Compromised tubes must be replaced to restore nominal instrument function.

7.2.3 *Mixed FID Heated Combustion Zone Systems*—Combining a FID and a heated combustion zone in series can afford the simultaneous detection of hydrocarbons and sulfur gases. Samples demonstrating high hydrocarbon interference can frequently be analyzed using this configuration.

8. Calibration

8.1 *Sample Introduction*—Using passivated or inert equipment, transfer an aliquot of calibration standard to the GC sample loop. The aliquot must be of sufficient size to completely flush and fill the sample loop. Generally, a sample size 10 times the volume of the sample loop and inlet line is sufficient. Inject the sample in the sample loop into the GC column and start the chromatographic program. Appropriate analyte concentrations should be selected for calibration.

8.2 *SCD Calibration*—Monthly or whenever maintenance is performed, a three-point calibration curve forced through zero and prepared for each analyte of interest is suggested and may be required for certain applications. Linearity confirmation is consistent with acceptable SCD performance.

8.2.1 When needed, linearity can be established according to the following procedure. For each concentration of analyte,

the standard is analyzed until three (3) consecutive trials yield a maximum range of 5 %. The average area for each point is calculated. A linear regression is performed for each component using the average area. For each calibration point, the determined concentration is calculated from the average areas. Linearity is confirmed when the determined amount is within 5 % of the actual amount of the analyte.

8.2.2 Establishment of linearity validates use of daily single-point calibration. When linearity cannot be established, a daily three-point calibration curve with end points bracketing anticipated analyte concentrations is suggested.

8.2.3 Typically daily, standards are analyzed until three (3) consecutive trials yield a maximum range of 5 %.

8.2.4 The SCD is an equimolar detector; therefore, response factors for all calibration components should be within 5 % of the response factor for hydrogen sulfide. Failure to satisfy this criteria indicates either calibration standard degradation or failure of the SCD heated combustion zone, flame ionization detector (FID), or related device.

8.2.5 Calculate the relative response factor for each sulfur compound:

$$F_n = (C_n/A_n) \quad (1)$$

where:

F_n = response factor of compound,

C_n = concentration of the sulfur compound in the mixture, and

A_n = peak area of the sulfur compound in the mixture.

The response factor (F_n) of each single sulfur compound should be within 5 % of F_n for hydrogen sulfide. Fig. 1 provides an example of a typical chromatogram and Table 4 shows the data and calibration report. Table 3 contains information useful for calibration calculations.

9. Procedure

9.1 Many operating conditions can be used to perform sulfur gas speciation and quantitation. Minimum criteria for acceptable operating conditions are as stated in 7.1. In addition, it is advisable and required for regulatory purposes to establish the limit of detection (LOD) for a SCD system.

9.2 *Sampling and Preparation of Samples*—Appropriate sampling procedures are critical for meaningful sulfur determination and must be tailored to the particular sample source.

9.2.1 *Samples*—Samples are delivered to the laboratory in Tedlar bags with polypropylene fittings or other inert fittings at atmospheric pressure, protected from heat and light. Samples normally must be analyzed within 24 h of sampling. Alternatively, samples are delivered to the laboratory in Silcosteel lined vessels or other passivated/lined vessel demonstrated to not degrade sulfur gas samples over 24 h. As part of a QA/QC program, passivated or lined vessels should periodically be examined for continued sulfur gas stability and acceptable sample carryover characteristics. Passivated or lined vessels may allow for reliable sample analysis after 24 h. In such cases, analysis is recommended within 7 days of collection.

9.3 *External Calibration*—Procedures delineated in 8.2 validate the use of a single-point calibration. At least once a day, analyze the calibration standard and determine standard

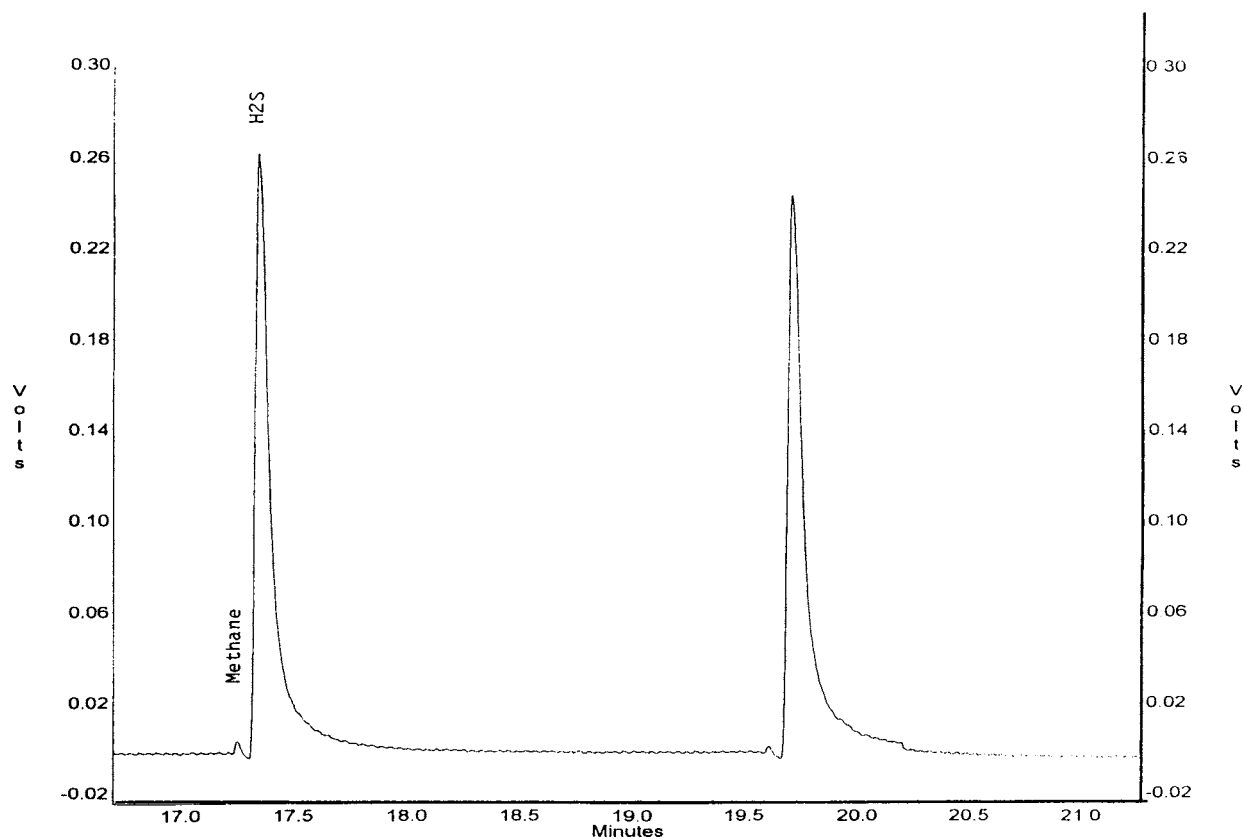


FIG. 4 Too Rich of a Combustion Flame Will Cause Methane Breakthrough

response factors. Typically, standards are analyzed until three (3) consecutive trials yield a maximum range of 5 %.

9.4 *Blank Analysis*—Confirmation of a lack of carry-over or contamination is recommended and may be required for certain applications. This is accomplished through analysis of a nitrogen or zero air blank. Observation of excessive amounts of high molecular weight volatile sulfur compounds is typical of injection valve deterioration.

9.5 *Sample Analysis*—The analysis of each sample in duplicate is strongly suggested and may be required for certain applications. Duplicate sample analysis will verify adequate SCD system conditioning and performance. Duplicate sample response for components present at or greater than 1 ppm (v/v) concentration in either analysis should generally be within ten (10) percent of the initial analysis to verify acceptable system performance. When the determined amount of any sulfur component exceeds the calibration range established under 8.2.2 a split injection should be used. Alternatively, samples may be diluted using UHP nitrogen or zero air as the diluant. Retention times for peaks in sample chromatogram are compared to those of peaks in the standard chromatograms to identify sulfur compounds. Compounds for which a standard is not available are conveniently quantified using the response factor from one of the calibrants. Run the analysis per the conditions specified in Table 1, or using other conditions satisfying the chromatographic performance criteria in 7.1.

Obtain the chromatographic data via a potentiometric record (graphic), digital integrator, or computer-based chromatographic data system. Examine the graphic display or digital data for any errors (for example, over-range component data).

9.6 *Quality Assurance*—The following quality assurance (QA) procedures are suggested and may be required in certain applications. These QA procedures will identify inaccuracy due to a compromised flame ionization detector or heated combustion zone or other SCD system component.

9.6.1 *Spiked Samples*—A spiked sample is analyzed each day as part of a QA/QC program. Spikes are prepared by quantitative addition of a mixed component calibration gas to a known volume of sample gas. Typically, 20 or 50 mL of a mixed component standard is added to a sample to give a final volume of 100 mL. Acceptable recoveries for components present at the greater of 5 ppmv or 5 % of the total volatile sulfur should fall within 10 % of the theoretical amounts to verify nominal system performance. Unacceptable recoveries indicate matrix interference or system malfunction. In many instances, when unacceptable recoveries are obtained, samples can be analyzed by dilution or other mitigation efforts.

9.6.2 *Calibration Standard Reanalysis*—A standard is re-analyzed after samples every day as part of a QA/QC program. All components should be within 10 % of the theoretical amounts based on the original standards. Unacceptable results typically are indicative of SCD combustion zone failure.

SCD 2.4 ppm H₂S in CH₄
 volume injected varied - 10/18/96

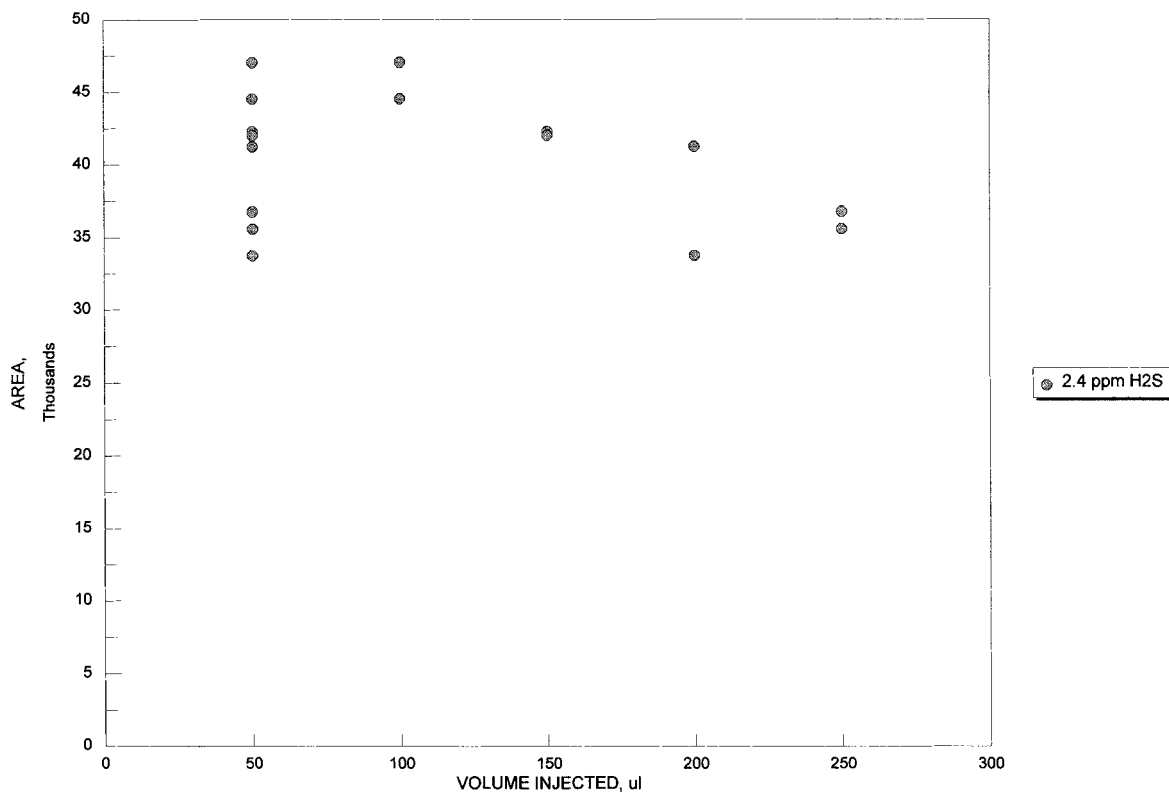


FIG. 5 Example of Matrix Interference. Changing the Sample Size Should Give a Change in Response

10. Calculations

10.1 Determine the chromatographic peak area for components and use the response factors obtained from the calibration run to calculate amounts of sulfurs present.

Example:

Assume 1.0 ppmv of dimethyl sulfide, DMS, injected into a 1.0 cc sample loop with no split.

1 ppmv DMS = 2.54 mg/M³ (Table 3)

2540 pg × 51.61 % S = 1310 picog S/peak

If area is found to be 15 850 counts—

response factor picograms (S/peak) is 1310/15 850 = 8.27 × 10⁻² (in terms of picograms sulfur per peak) or

response factor (ppmv DMS sample) = 1.0/15 850 = 63 × 10⁻⁶ (in terms of ppmv of sulfur compound in sample)

NOTE 3—Since detector response is proportional to weight sulfur, all mono sulfur compounds (COS, H₂S, DMS, etc.) will have approximately the same response factor for picograms S or ppmv (see 8.2.2).

Alternatively, concentration of volatile sulfur compounds is calculated in ppm (v/v) by the following:

$$\text{Analyte concentration, ppm} = \frac{\text{pk}_{\text{sample}}}{\text{pk}_{\text{standard}}} \times \text{Std} \quad (2)$$

where:

analyte concentration = concentration of individual sulfur compounds or SO₂,

pk_{sample} = peak area in the sample,

pk_{std} = peak area in the standard, and

Std = concentration of analyte in the standard, ppm.

Peak heights can be substituted for peak areas.

Total volatile sulfur is the sum of all identified and unidentified sulfur compounds.

10.2 Recoveries for the total volatile sulfur or each component in spiked samples are calculated by the following:

SCD 2.4 ppm H₂S in CH₄
 volume injected varied - 10/18/96

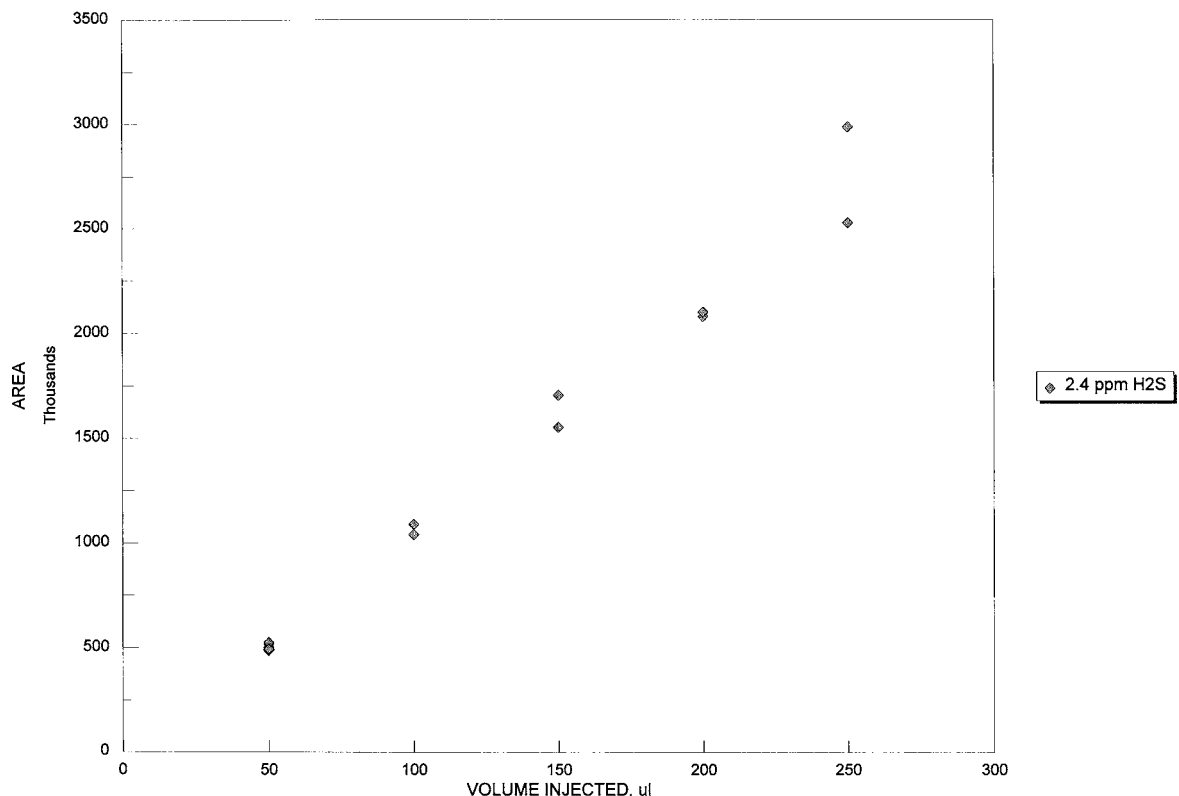


FIG. 6 Example of Typical Response Curve with Varying Sample Size

TABLE 3 Sulfur Gas Standard

Compound	Mol. Wt.	Density	BP°C	%S	(Conversion) Mg/M3 per PPMV
Hydrogen sulfide (H ₂ S)	34.08	1.1857	—	94.08	1.39
Carbonyl sulfide (COS)	60.08	1.24	—	53.37	2.46
Methanethiol (MeSH)	48.110	0.8665	6.2	66.65	1.97
Ethanethiol (EtSH)	62.134	0.8391	35.0	51.61	2.54
Dimethylsulfide (DMS)	62.134	0.8483	37.3	51.61	2.54
Carbon disulfide (CS ₂)	76.14	—	—	84.23	3.11
2-Propanethiol (iPrSH)	76.160	0.8143	52.6	42.10	3.11
t-Butanethiol (tBSH)	64.220	0.8002	65.0	49.93	2.62
1-Propanethiol (nPrSH)	76.160	0.8415	67.0	42.10	3.11
Methylethylsulfide (MES)	76.160	0.8422	67.0	42.10	3.11
Thiophene (TP)	84.14	1.07	84.16	38.03	3.44
s-Butanethiol (s-BuSH)	90.186	0.8299	85.0	35.56	3.69
i-Butanethiol (i-BuSH)	90.186	0.8343	88.7	35.56	3.69
Diethylsulfide (DES)	90.190	0.8362	92.0	35.55	3.69
n-Butanethiol (n-BuSH)	90.186	0.8416	98.5	35.56	3.69
Dimethyldisulfide (DMDS)	94.200	1.0625	109.7	68.08	3.85
Diethyldisulfide (DEDS)	122.252	0.9931	154.0	52.46	5.00

TABLE 4 Calibration Table

SIEVERS 8 PTUBES NEW DET—MEGABORE/20PSIG He 5/6/91
 SPLITLESS Calibration file: DATA:SVPT.Q Last Update: 24 Jul 91
 5:37 pm Reference Peak Window: 5.00 % of Retention Time Non-
 Reference Peak Window: 5.00 % of Retention Time Sample Amount:
 0.000 Uncalibrated Peak RF: 60.00e-6 Multiplier: 1.000

Ret Time	Ph#	Signal Descr	Amt PPMV	cvl RespFact	Pk-Type Partial Name
1.461	1	GC Signal 1	0.9100	1 59.60e-6	1 H2S
1.595	2	GC Signal 1	0.2610	1 36.92e-6	1 COS
2.861	3	GC Signal 1	0.3570	1 50.11e-6	1 MTM
3.529	4	GC Signal 1	0.4150	1 50.28e-6	1 ETM
3.809	5	GC Signal 1	0.4943	1 49.02e-6	1 DMS
4.185	6	GC Signal 1	0.2289	1 0001001	1 CS2
4.481	7	GC Signal 1	0.3904	1 50.04e-6	1 1PM
5.179	8	GC Signal 1	0.6140	1 49.99e-6	1 TBM
5.521	9	GC Signal 1	2.600	1 50.00e-6	1 MES
6.738	10	GC Signal 1	0.9870	1 49.99e-6	1 SBM
7.129	11	GC Signal 1	1.225	1 48.81e-6	1 DES
7.868	12	GC Signal 1	1.135	1 49.99e-6	1 NBM
7.912	13	GC Signal 1	0.07660	1 0.0001000	1 DMDS
9.017	14	GC Signal 1	1.558	1 49.99e-6	1 THT

$$\text{Recovery (\%)} = \frac{\text{SM}}{(\text{SA})(\text{DF}_1) + (\text{SS})(\text{DF}_2)} \times 100 \quad (3)$$

where:

SM = measure spiked sample concentration in ppm (v/v),

SA = the average sample concentration from duplicate analysis of the sample in ppm (v/v),

SS = Concentration of the analyte used to spike the sample in ppmv,

DF₁ = dilution factor for the sample, and

DF₂ = dilution factor for the standard.

Recoveries are only calculated for components in the standard used to spike the sample. The total recovery for the spike is calculated according to the above equation using only components in the standard used to perform the spike.

10.3 Recoveries for post sample reanalyzed standards are calculated by the following:

$$\text{QA/QC Recovery (\%)} = \frac{\text{Calibration Value} - \text{Measured Value}}{\text{Calibration Value}} \times 100 \quad (4)$$

11. Report

11.1 Report the identification and concentration of each individual sulfur compound. The sum of all sulfur components detected to the nearest picogram, calculated as sulfur (pg S) can be used to calculate the total sulfur. Alternatively, the

results may be reported in ppm (v/v) when required by using the alternative calculations contained in 10.1.

12. Precision and Bias

12.1 *Precision*—The precision of this test method as determined by the statistical examination of the inter-laboratory test results is as follows:

12.1.1 *Repeatability*—The difference between successive test results obtained by the same operator with the same apparatus under constant operating conditions on identical test material would, in the long run, in the normal and correct operation of the test method, exceed the following values by only one case in twenty. (Experimental results to be determined.)

12.1.2 *Reproducibility*—The difference between two single and independent results obtained by different operators working in different laboratories on identical test material would, in the long run, exceed the following values only one case in twenty. (Experimental results to be determined.)

12.2 *Bias*—The procedure in Test Method D5504 for the analysis of sulfur compounds in petroleum and petroleum products by gas chromatography has no bias.

13. Keywords

13.1 chemiluminescence detection; gas chromatography; sulfur compounds

APPENDIXES

(Nonmandatory Information)

X1. PROTOCOL FOR COMPRESSED GAS CALIBRATION STANDARDS

This protocol was developed to assist compressed gas sulfur standard users. It can provide calibration gas traceability to a NIST, NMI, or similar standard reference material. This protocol requires the determination of the speciated and total sulfur using a NIST or NMI hydrogen sulfide SRM or a NTRM as the primary reference. This procedure will insure uniformity in measurement of sulfur content. This protocol was developed by compressed gas vendors and should be submitted to vendors when calibration gas is ordered.

X1.1 A standard is analyzed according to Test Method D5504. The GC temperature program is designed to elute all sulfur species up to and including di-n-propyl sulfide. A minimum of three consecutive data points are collected with the necessary precision to support the reported analytical accuracy. The necessary precision is achieved with a percent relative standard deviation (% RSD) calculated from a minimum of three consecutive data points, less than or equal to one percent. An average area for each component and the total sulfur area is calculated using all consecutive analyses.

X1.2 A hydrogen sulfide standard reference material is analyzed under identical conditions used in the analysis of the standard. Acceptable hydrogen sulfide reference standards

include NIST or NMI traceable SRMs or NTRMs. A minimum three consecutive data points are collected with the necessary precision to support the reported analytical accuracy. An average area of the hydrogen sulfide is calculated using all consecutive analysis:

X1.3 The values for individual sulfur components and the total sulfur amount are calculated according to the formula:

$$\text{Sulfur calculated concentration} = \frac{\text{Average area as calculated in step 1}}{\text{Average area as calculated in step 2}} \times \text{H}_2\text{S Std. Conc.} \quad (\text{X1.1})$$

X1.4 The analysis for total volatile sulfur and individual components calculated as hydrogen sulfide (X1.1-X1.3) is performed at least twice, with a minimum 48 hour incubation period between the two analyses. The difference in percent between the two values, for total volatile sulfur and individual components calculated as hydrogen sulfide must be less than 2%. This is necessary to assure product stability. The reported total and individual sulfur concentrations are the value obtained in the second analysis.

X1.5 The values for total volatile sulfur and individual components are reported on the certificate of analysis as follows:

X1.5.1 The values for the total volatile sulfur and individual components from both the first and second analysis in **X1.4**, along with the date of analyses.

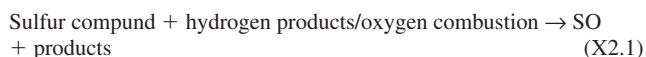
X1.5.1.1 The cylinder number, concentration and NIST or NMI SRM/NTRM batch ID from the NIST reference standard used in the standard analysis.

X1.5.1.2 The total sulfur reported must include all components including any unknowns. The total of the unknowns shall also be reported in ppm.

X2. CHEMILUMINESCENCE REACTION MODELS

Gas chromatography with sulfur chemiluminescence detection is a powerful means to separate and measure sulfur compounds in complex samples including natural gas, refinery fuel gas, landfill gas and other gaseous fuels **(1-3)**.⁵ Two mechanisms have been proposed as the basis for SCD operation.

X2.1 *Model 1*—One chemical reaction proposed as the basis for SCD operation is shown below **(4-9)** some background references on sulfur chemistry and chemiluminescence are also given **(10-14)**:



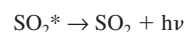
where:

h_ν = light energy at 300-400 nm.

According to this mechanism, sulfur monoxide and the other combustion products are transferred to a reaction cell. Ozone produced in an ozonator is added to the reaction cell where it reacts with sulfur monoxide. The emitted light is measured

using a photomultiplier tube. A vacuum maintains the reaction cell at or below 10 mm of pressure. This prevents the loss of sulfur monoxide and minimizes loss of response due to collisional quenching.

X2.2 *Model 2*—A second reaction mechanism proposed as the basis for SCD operation is depicted below **(13-15)**:



According to this mechanism, sulfur compounds are combusted to SO_2 . Sulfur dioxide is reduced, in the presence of excess hydrogen to H_2S . Hydrogen sulfide is transferred to a reaction cell. Ozone produced in an ozonator is added to the reaction cell where it reacts with hydrogen sulfide to create excited state sulfur dioxide. Relaxation of sulfur dioxide to the ground state releases a photon. The emitted light is measured using a photomultiplier tube. A vacuum maintains the reaction cell at or below 10 mm of pressure. This minimizes the loss of response due to collisional quenching of excited state sulfur dioxide.

⁵ The boldface numbers in parentheses refer to the list of references at the end of this standard.

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